- Supply voltage: 1.5 V to 5 V
- $\mathbf{~} \mathbf{2 0} \mathbf{~ m W}$ adjustable output power
- 28 dB gain at 450 MHz
- 21 dB gain at 900 MHz
- $50 \Omega$ matched input and output
- Bias pin to adjust the amplification class
- Power down


## DESCRIPTION

The TSH690 is a wide band RF amplifier, designed in advanced bipolar process. At 450 MHz , it features 28 dB gain and $+13.5 \mathrm{dBm}(20 \mathrm{~mW})$ output power at 3 V . At 900 MHz , it features 23 dB gain and $+15.5 \mathrm{dBm}(35 \mathrm{~mW})$ output power at 3 V .
The pin 8 allows a bias current adjust, setting the RF output level and the amplifier behaviour. It allows using the TSH690 from the linear A-class trough the AB-class to power-down mode.
The TSH690 is suited to drive power amplifiers in cellular phones (GSM, TDMA) for which the 'turn-on time' is controlled by a voltage ramp.
The more than 20 mW output power makes the TSH690 dedicated as output stage for 433 MHz and 868 MHz ISM transmitters.

## APPLICATIONS

- 433 MHz and 868 MHz ISM transmitters
- Telemetering systems
- Remote controls
- Cordless Telephones
- Driver for cellular phones
- Wide band applications

ORDER CODE

| Part Number | Temperature Range | Package |
| :--- | :---: | :---: |
|  |  | $\mathbf{D}$ |
| TSH690ID | $-40,+85^{\circ} \mathrm{C}$ | $\bullet$ |

[^0]
## PACKAGE



PIN CONNECTIONS (top view)


## SCHEMATIC DIAGRAM



## ABSOLUTE MAXIMUM RATINGS

| Symbol | Parameter | Value | Unit |
| :---: | :--- | :---: | :---: |
| $\mathrm{V}_{\mathrm{CC} 1}, \mathrm{~V}_{\mathrm{CC} 2}, \mathrm{~V}_{\text {bias }}$ | Supply Voltage \& Bias Voltage | 5.5 | V |
| RF in | RF Input Power | +10 | dBm |
| RF out | RF Output Power | +21 | dBm |
| $\mathrm{T}_{\text {oper }}$ | Operating Free Air Temperature Range | -40 to +85 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {stg }}$ | Storage Temperature Range | -65 to +150 | ${ }^{\circ} \mathrm{C}$ |

OPERATING CONDITIONS

| Symbol | Parameter | Value | Unit |
| :---: | :--- | :---: | :---: |
| $\mathrm{V}_{\mathrm{CC} 1}, \mathrm{~V}_{\mathrm{CC} 2}$ | Supply Voltages | 1.5 to 5 | V |
| $\mathrm{~V}_{\text {bias }}$ | Bias Voltage | 0 to 5 | V |
| $\mathrm{RF}_{\mathrm{sr}}$ | RF Signal Range | 40 to 1000 | MHz |

## ESD SENSITIVE DEVICE <br> Handling Precautions Required

## ELECTRICAL DC CHARACTERISTICS

Tamb $=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}$ connected to $\mathrm{V}_{\text {bias }}, \mathrm{Z}_{\mathrm{L}}=50 \Omega$ (unless otherwise specified)

| Parameter | Min. | Typ. | Max. | Unit |
| :--- | :---: | :---: | :---: | :---: |
| Supply Current |  |  |  |  |
| Vcc $=2 \mathrm{~V}$ |  | 29 |  |  |
| Vcc $=2.7 \mathrm{~V}$ |  | 46 |  | mA |
| Vcc $=3 \mathrm{~V}$ | 33 | 53 |  |  |
| Vcc $=4 \mathrm{~V}$ |  | 79 |  |  |
| Vcc $=5 \mathrm{~V}$ |  |  | 105 |  |
| Rth-(j-a): Junction Ambient Thermal Resistance for SO-8 Package | 140 |  | 180 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

## TSH690 DISSIPATION CONSIDERATIONS

In order to respect the dissipation limitation of the package, you should consider the following equation:

$$
\mathrm{T}_{\mathrm{j}}-\mathrm{T}_{\mathrm{amb}}=\mathrm{P}_{\mathrm{d}} \bullet \mathrm{R}_{\mathrm{thf}(-\mathrm{a})}
$$

with:
$\mathrm{R}_{\mathrm{th}(\mathrm{ja)}}=$ junction ambient thermal resistance
$\mathrm{T}_{\mathrm{j}}\left({ }^{\circ} \mathrm{C}\right)=$ max. junction temperature $\left(150^{\circ} \mathrm{C}\right)$
$\mathrm{T}_{\text {amb }}\left({ }^{\circ} \mathrm{C}\right)=$ ambient temperature
$P_{d}(W)=$ maximum dissipated power
The respect of this condition forms a safe area on the following figure:

Figure 1 : Dissipation capability vs T ambient


If VBIAS is DC connected to VCC, the operating temperature can be directly determined without
determining ICC, thanks to the direct reading curve:

Figure 2 : Maximum $\mathrm{T}_{\text {amb }}$ vs $\mathrm{V}_{\mathrm{CC}}$


In applications using a duty cycle, the average dissipation is less than in continuous mode. The following figure gives the relation beetween the dissipated power and the duty cycle.
Figure 3 : Dissipation vs Duty cycle


## ELECTRICAL CHARACTERISTICS AT 450 MHz

Tamb $=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}} \& \mathrm{~V}_{\text {bias }}=+2.7 \mathrm{~V}, \mathrm{Z}_{\mathrm{L}}=50 \Omega, \mathrm{f}=450 \mathrm{MHz}$ (unless otherwise specified)

| Parameter $\left.{ }^{1}\right)$ | Min. | Typ. | Max. | Unit |
| :--- | :---: | :---: | :---: | :---: |
| Power gain S21 ( $\left.\mathrm{P}_{\text {in }}=-20 \mathrm{dBm}\right)$ | 20 | 23 | 30 | dB |
| Output Power 1dB Compression | 8 | 12 |  | dBm |
| 3rd Order Intercept Point $(\mathrm{f}=430 \mathrm{MHz})$ | 16 | 22 |  | dBm |
| Reverse Isolation S12 $(\mathrm{f}=400 \mathrm{MHz})$ |  | -46 |  | dB |
| Input Return Loss S11 | -10 | -15 |  | dB |
| Noise Figure |  | 4.5 | dB |  |

1. All min. and max. parameters of this table are garanteed by correlation with 900 MHz tests.

## ELECTRICAL CHARACTERISTICS AT $900 \mathbf{M H z}$

Tamb $=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}} \& \mathrm{~V}_{\text {bias }}=+3 \mathrm{~V}, \mathrm{Z}_{\mathrm{L}}=50 \Omega, \mathrm{f}=900 \mathrm{MHz}$ (unless otherwise specified)

| Parameter ${ }^{1)}$ | Min. | Typ. | Max. | Unit |
| :--- | :---: | :---: | :---: | :---: |
| Power gain S21 ( $\left.\mathrm{P}_{\text {in }}=-20 \mathrm{dBm}\right)$ | 19 | 21 |  | dB |
| Output Power at 1dB compression point | +12 | +14.3 |  | dBm |
| Output power, Pin $=-7 \mathrm{dBm}$ | +10 | +11.7 |  | dBm |
| 3rd Order Intercept Point |  | +25 |  | dBm |
| Reverse Isolation S12 |  | -35 |  | dB |
| Input Return Loss S11 |  | -14 |  | dB |
| Output Return Loss S22 |  | -4.5 | dB |  |
| Noise figure |  | 5.4 | dB |  |

1. All min. and max. parameters of this table are garanteed by test.

SCATTERING PARAMETERS MEASUREMENT (Reference waves planes at package leads)


TEST CONDITIONS $\mathrm{V}_{\mathrm{CC} 1}, \mathrm{~V}_{\mathrm{CC} 2}, \mathrm{~V}_{\text {bias }}=+2 \mathrm{~V}$, Pin $=-40 \mathrm{dBm}, \mathrm{T}_{\text {amb }}=25^{\circ} \mathrm{C}$

| Freq | S11 |  | S21 |  | S12 |  | S22 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MHz | Mag | Ang | Mag | Ang | Mag | Ang | Mag | Ang |
| 40 | 0.642 | -22.0 | 6.319 | 5.0 | 0.003 | -126.5 | 0.715 | -54.7 |
| 50 | 0.615 | -25.7 | 6.406 | 7.1 | 0.008 | 170.7 | 0.631 | -64.7 |
| 100 | 0.537 | -41.3 | 7.643 | 7.7 | 0.002 | 70.1 | 0.369 | -91.3 |
| 150 | 0.490 | -55.6 | 9.353 | 3.1 | 0.004 | -141.9 | 0.253 | -100.9 |
| 200 | 0.464 | -68.0 | 11.502 | -5.7 | 0.007 | -117.3 | 0.202 | -100.9 |
| 250 | 0.428 | -79.0 | 13.856 | -18.0 | 0.003 | 162.3 | 0.203 | -92.7 |
| 300 | 0.413 | -92.1 | 16.229 | -33.4 | 0.005 | 142.1 | 0.209 | -87.6 |
| 350 | 0.373 | -101.5 | 18.019 | -51.2 | 0.008 | 101.4 | 0.263 | -89.4 |
| 400 | 0.334 | -106.7 | 19.110 | -70.1 | 0.008 | 115.2 | 0.326 | -99.7 |
| 450 | 0.312 | -111.5 | 19.159 | -90.3 | 0.008 | 169.9 | 0.382 | -112.1 |
| 500 | 0.290 | -112.5 | 18.154 | -108.0 | 0.008 | 111.5 | 0.395 | -122.9 |
| 550 | 0.302 | -114.5 | 16.778 | -124.8 | 0.010 | 92.1 | 0.425 | -130.0 |
| 600 | 0.324 | -118.2 | 15.075 | -140.5 | 0.015 | 93.6 | 0.424 | -139.6 |
| 650 | 0.335 | -122.9 | 13.482 | -153.6 | 0.011 | 109.6 | 0.427 | -150.8 |
| 700 | 0.349 | -129.6 | 11.992 | -165.5 | 0.011 | 101.7 | 0.425 | -159.0 |
| 750 | 0.368 | -135.0 | 10.750 | -177.2 | 0.019 | 82.4 | 0.414 | -169.5 |
| 800 | 0.366 | -142.1 | 9.453 | 173.4 | 0.011 | 79.5 | 0.413 | -177.8 |
| 850 | 0.373 | -147.9 | 8.598 | 165.0 | 0.015 | 60.2 | 0.432 | 176.2 |
| 900 | 0.374 | -154.1 | 7.783 | 155.8 | 0.013 | 89.7 | 0.438 | 166.4 |
| 950 | 0.381 | -159.0 | 7.117 | 146.7 | 0.017 | 111.3 | 0.447 | 160.8 |
| 1000 | 0.377 | -165.8 | 6.500 | 138.9 | 0.013 | 82.2 | 0.462 | 155.1 |

TEST CONDITIONS $\mathrm{V}_{\mathrm{CC} 1}, \mathrm{~V}_{\mathrm{CC} 2}, \mathrm{~V}_{\text {bias }}=+3 \mathrm{~V}$, Pin $=-40 \mathrm{dBm}, \mathrm{T}_{\text {amb }}=25^{\circ} \mathrm{C}$

| Freq | S11 |  | S21 |  | S12 |  | S22 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MHz | Mag | Ang | Mag | Ang | Mag | Ang | Mag | Ang |
| 40 | 0.616 | -23.3 | 9.237 | 6.2 | 0.002 | -135.8 | 0.733 | -56.9 |
| 50 | 0.595 | -27.0 | 9.402 | 7.9 | 0.005 | -169.5 | 0.651 | -67.7 |
| 100 | 0.513 | -43.4 | 11.263 | 6.5 | 0.006 | -153.8 | 0.381 | -101.7 |
| 150 | 0.470 | -57.7 | 13.566 | 0.9 | 0.006 | 94.5 | 0.227 | -119.1 |
| 200 | 0.436 | -71.1 | 16.434 | -8.6 | 0.007 | 155.8 | 0.156 | -117.5 |
| 250 | 0.402 | -82.2 | 19.416 | -21.3 | 0.007 | 154.1 | 0.134 | -100.3 |
| 300 | 0.382 | -95.0 | 22.265 | -36.6 | 0.005 | 7.2 | 0.135 | -75.7 |
| 350 | 0.343 | -103.3 | 24.337 | -53.7 | 0.008 | 40.6 | 0.193 | -78.0 |
| 400 | 0.302 | -109.7 | 25.564 | -71.8 | 0.010 | 125.9 | 0.269 | -86.1 |
| 450 | 0.279 | -114.8 | 25.594 | -91.2 | 0.008 | 167.1 | 0.316 | -100.6 |
| 500 | 0.271 | -114.0 | 24.292 | -108.3 | 0.011 | 120.2 | 0.356 | -111.0 |
| 550 | 0.280 | -116.1 | 22.527 | -124.7 | 0.013 | 101.0 | 0.396 | -119.3 |
| 600 | 0.306 | -119.8 | 20.511 | -140.1 | 0.005 | 89.9 | 0.404 | -131.3 |
| 650 | 0.315 | -125.5 | 18.282 | -153.2 | 0.006 | 107.2 | 0.400 | -142.6 |
| 700 | 0.330 | -131.1 | 16.311 | -165.1 | 0.007 | 78.9 | 0.406 | -151.6 |
| 750 | 0.333 | -136.2 | 14.604 | -177.1 | 0.012 | 84.5 | 0.398 | -160.4 |
| 800 | 0.343 | -142.5 | 12.860 | 173.6 | 0.017 | 76.0 | 0.399 | -170.5 |
| 850 | 0.346 | -148.0 | 11.668 | 165.1 | 0.014 | 90.8 | 0.411 | -178.8 |
| 900 | 0.354 | -155.1 | 10.579 | 156.0 | 0.018 | 75.6 | 0.413 | 170.9 |
| 950 | 0.347 | -159.6 | 9.652 | 147.0 | 0.013 | 66.6 | 0.439 | 165.2 |
| 1000 | 0.355 | -166.2 | 8.775 | 139.2 | 0.018 | 75.3 | 0.459 | 157.3 |

TEST CONDITIONS $\mathrm{V}_{\mathrm{CC} 1}, \mathrm{~V}_{\mathrm{CC} 2}, \mathrm{~V}_{\text {bias }}=+4 \mathrm{~V}$, Pin $=-40 \mathrm{dBm}, \mathrm{T}_{\text {amb }}=25^{\circ} \mathrm{C}$

| Freq | S11 |  | S21 |  | S12 |  | S22 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MHz | Mag | Ang | Mag | Ang | Mag | Ang | Mag | Ang |
| 40 | 0.614 | -23.1 | 11.023 | 6.9 | 0.002 | 107.6 | 0.726 | -54.4 |
| 50 | 0.590 | -27.4 | 11.248 | 7.9 | 0.003 | -111.3 | 0.646 | -65.1 |
| 100 | 0.508 | -44.6 | 13.262 | 4.5 | 0.004 | -47.0 | 0.366 | -97.6 |
| 150 | 0.465 | -59.9 | 15.736 | -2.0 | 0.006 | -62.5 | 0.206 | -110.4 |
| 200 | 0.429 | -72.0 | 18.727 | -11.5 | 0.003 | 97.7 | 0.130 | -104.3 |
| 250 | 0.396 | -83.4 | 21.837 | -24.2 | 0.002 | -135.5 | 0.108 | -78.6 |
| 300 | 0.371 | -94.7 | 24.804 | -39.3 | 0.009 | 154.7 | 0.136 | -56.7 |
| 350 | 0.335 | -103.8 | 26.854 | -56.0 | 0.006 | 135.2 | 0.191 | -64.3 |
| 400 | 0.295 | -109.9 | 28.077 | -73.6 | 0.003 | 139.7 | 0.262 | -75.2 |
| 450 | 0.275 | -114.8 | 28.113 | -92.5 | 0.010 | 97.0 | 0.321 | -85.8 |
| 500 | 0.265 | -114.8 | 26.710 | -109.4 | 0.007 | 111.8 | 0.335 | -98.2 |
| 550 | 0.282 | -117.0 | 24.831 | -125.5 | 0.007 | 93.8 | 0.389 | -108.5 |
| 600 | 0.296 | -120.3 | 22.620 | -140.8 | 0.007 | 110.0 | 0.393 | -121.0 |
| 650 | 0.314 | -124.7 | 20.235 | -154.1 | 0.005 | 85.1 | 0.402 | -131.7 |
| 700 | 0.321 | -131.5 | 18.081 | -166.2 | 0.010 | 93.2 | 0.388 | -143.9 |
| 750 | 0.334 | -135.8 | 16.178 | -178.0 | 0.012 | 106.1 | 0.390 | -153.8 |
| 800 | 0.339 | -143.8 | 14.235 | 172.5 | 0.010 | 74.1 | 0.377 | -162.4 |
| 850 | 0.348 | -149.4 | 12.941 | 164.1 | 0.014 | 57.9 | 0.392 | -170.4 |
| 900 | 0.340 | -157.5 | 11.693 | 154.9 | 0.014 | 80.2 | 0.402 | 179.5 |
| 950 | 0.352 | -161.0 | 10.670 | 145.7 | 0.006 | 87.4 | 0.409 | 171.4 |
| 1000 | 0.341 | -166.8 | 9.683 | 137.6 | 0.016 | 50.0 | 0.433 | 163.3 |

Figure 4 : Demonstration board schematic


## TSH690 DESCRIPTION

The TSH690 is a 2 transistor stages amplifier running within the $40 \mathrm{MHz}-1 \mathrm{GHz}$ frequency band featuring a gain of 28 dB at 433 MHz . The TSH690 is $50 \Omega$ input/output internally matched from 300 MHz to 1000 MHz . The open collector output requires an inductive load for the impedance matching and also to reach an output power of $+13,5 \mathrm{dBm}$ at 3 V and +18 dBm at 4 V . A bias control pin allows tuning of current consumption and amplification mode.
As the matter of fact, when the bias pin is tied to the supply voltage, amplification is linear (Class A) while a lower voltage leads to a Class A-B amplification featuring a better efficiency. If the control voltage is grounded, the TSH690 is set in Pow-er-down mode without current consumption.

## MATCHING THE OUTPUT WITH L2

Within the $300-1000 \mathrm{MHz}$ band, although the circuit is matched, the output return loss (S22) can be improved by adapting the value of the inductor L2. This inductor is connected between the RF output and $\mathrm{V}_{\mathrm{CC} 2}$.
$\mathrm{L} 2=56 \mathrm{nH}$ gives an output return loss of -19 dB at 450 MHz .
$\mathrm{L} 2=10 \mathrm{nH}$ gives an output return loss of -8 dB at 900 MHz .
In a 433 or 450 MHz transmitter application, L1 and L 2 can be optimized to reduce the second harmonic by choosing $\mathrm{L} 1=33 \mathrm{nH}$ and $\mathrm{L} 2=15 \mathrm{nH}$.
Below 300 MHz , using the S-parameters matrix, specific input/output matching networks can be calculated to maximize electrical performances.

## DC BLOCKING

Because input/output are respectively internal/external biased, DC blocks (C1, C2) are recommended on both RF ports to guarantee a DC isolation from the next cells. Above $500 \mathrm{MHz}, 100 \mathrm{pF}$ is suggested whereas below, 1 nF is better and far below (less than 100 MHz ), 10 nF is prefered.

## BIASING

The amplifier can operate in the range of 1.5 V to 5 V and offers a bias current adjust function (Vbias pin ) which enables the trimming of the RF output power (AB class Amplifier) by tuning a series variable resistor (Rbias).
When Vbias is wired to the Vcc rail, the current consumption is maximized getting the best linearity (A class Amplifier) whereas biasing to Ground, the IC is set in power down mode.
For higher supply voltage than 4 V to reach high output power, the serial resistor (R1) is strongly recommended to increase the efficiency of the amplifier and therefore reduce the thermal dissipation of the circuit.

## DECOUPLING

As with any RF devices, the supply voltage decoupling must be done carefully using a 1 nF bypass capacitor (C3, C5) placed as close as possible to the device pins and could be also improved by adding a 150 nH RF choke inductance (L1). Concerning the Vbias pin, a 10 nF decoupling capacitor (C4) is recommended while placing on board is not critical. Note that Surface Mounted Devices (SMD) components are prefered for RF applications due to the right behaviour in high frequencies while low inductor values (few 10 nH ) can be printed on board.

## DETERMINING VBIAS AND R1 AT 450 MHz

Using the 450 MHz curves, you can easily determine $\mathrm{V}_{\text {BIAS }}$ voltage and R1 to obtain the desired power gain S21.
For a given gain $\mathrm{S}_{21}$ and a given supply voltage $\mathrm{V}_{\mathrm{CC}}$, you can determine the corresponding $\mathrm{V}_{\text {BIAS }}$.using the curve 'Gain vs $\mathrm{V}_{\text {BIAS }}$ ' in the '450 MHz operation' section.
It's generally more convenient to supply the Vbias from $\mathrm{V}_{\mathrm{CC}}$ than generate a separate voltage. You just need to add the R1 resistor beetween the $V_{\text {BIAS }}$ pin and $V_{C C}$.
Using the curve 'Supply current vs Bias voltage' you can determine the current $I_{\text {BIAS }}$ corresponding to a $\mathrm{V}_{\text {BIAS }}$. R1 can calculated by:
$R 1=\left(V_{C C}-V_{B I A S}\right) / I_{B I A S}$.
One the same curve, you will find the total current supply Icc versus the biasing conditions.

Figure 5 : Demo board silk screen (not to scale)


450 MHz operation (L2 = $\mathbf{5 6} \mathbf{n H}$ )

GAIN vs FREQUENCY


INPUT RETURN LOSS


## OUTPUT RETURN LOSS



GAIN vs VBIAS VOLTAGE


900 MHz operation (L2 = 10 nH )

GAIN vs FREQUENCY


INPUT RETURN LOSS


## OUTPUT RETURN LOSS



OUTPUT POWER vs INPUT POWER


## OUTPUT POWER vs VBIAS



## Other curves

## REVERSE ISOLATION vs FREQUENCY



SUPPLY CURRENT vs BIAS VOLTAGE


## ASK TRANSMITTER USING THE TSH690

## Application purpose

The purpose is to use the TSH690 as a ASK transmitter for remote control applications taking benefits of the 2 stages architecture, the bias control pin and output power capability.
The first transistor stage is devoted to the oscillator by the meaning of a Surface Acoustic Wave (SAW) resonator while the second stage realizes the power amplification to drive antennas including the impedance matching.
Modulation is insured by applying the modulating signal onto the bias pin of TSH690 to get an amplitude modulation.

Figure 7 : Saw transmitter schematic


## Oscillator Considerations

The oscillator frequency is given by the SAW resonator which is connected between pins 5 \& 7 of the TSH690 to ensure a well-known Colpitts architecture with 2 capacitors C 1 and C2. Capacitor C2 is a small value one and, depending on PCB, could be directly obtained from parasitics of microstrip lines. Center frequency is tuned with the trimmer capacitor C1.
Note that the pin 7 is internally connected to an integrated self inductor L1 which is wired to the collector of the first stage transistor. A resistor R1 is placed to avoid resonance between L1 and C1 but also to adjust the current consumption of the oscillator.
Moreover, start-up conditions and output harmonics levels are related to the R1 value, so that its recommended to use a potentiometer for R1.

By tuning R1 and C1, stability of the circuit can be guaranted disregarding the load impedance of the output stage.

## Output Stage

The output matching is defined for a $50 \Omega$ load impedance by adding a 100 nH self-inductor L2 as load to the open collector of the output stage while capacitor C3 is just placed as a DC block with the antenna.

In such described conditions, output power on fundamental reaches more than +13 dBm under 3 V with an average current consumption of 50 mA featuring 2nd \& 3rd harmonics levels respectively of -18 dBc et -27 dBc .

## Modulation

As a result of applying a modulating signal to the bias pin (pin 8), the TSH690 features an amplitude modulation up to the On-Off-Keying when the modulating signal is digital.

A series resistor R2 can be added on pin 8 to change biasing conditions but also oscillating conditions and finally the available output power. In most of applications, this resistor can be omitted.

In the case of digital modulation control, when a ' 0 ' logic level is applied on pin 8, the circuit in set in Standby mode during which the oscillator is stopped whereas during a ' 1 ' logic level, the circuit radiates RF wave due to oscillator running mode. The maximum data rate of modulating signal is given by the oscillator turn-on time which is typically of $200 \mu \mathrm{~s}$ to reach the nominal operating frequency and amplitude. Note that the turn-off time is negligeable. Thus, it is recommended to use a data rate of $2400 \mathrm{~b} /$ s to keep a duty cycle of $25 \%$ (T_ON~200 $\mu \mathrm{s}$, T_OFF~ $(400+200) \mu \mathrm{s}$ ). For a higher data rate (maximum of $4800 \mathrm{~b} / \mathrm{s}$ ), duty cycle on transmission side decreases drastically so that it is recommended to use a monostable on reception side to recover a correct $50 \%$ duty cycle. In order to decrease the spectrum shape of transmission, a simple low-pass filter can be added in front of pin 8 to attenuate high level harmonics of the modulating signal.

Figure 8 : PCB component side (not to scale)


## Routing Requirements

Supply voltages : as well as any RF design boards, decoupling of supply voltages requires carefully routing. So, the output stage features a $10 \mu \mathrm{~F}$ tank capacitor to smooth current peaks and 2 decoupling capacitors of 1 nF and 100pF avoiding a RF feedback to the supply.
The oscillator biasing (pin 7) requires a RF choke self inductance of 56 nH in series with R1 and also a grounded decoupling capacitor of 1 nF .
Ground: The ground routing has to be done in the manner of decreasing resistive and inductive parasitics effects to guarantee the best equipotential of the electrical ground node. By using microstrip lines, bottom and top ground planes must be connected via through holes in respect with a distance shorter than 10 times the running wavelength. In practice, with a standard epoxy substrate ( $\operatorname{Er} \sim 4,5$ ), to run at about 450 MHz , distance between 2 vias must not exceed $\sim 3 \mathrm{~cm}$. By using a standard 2.54 mm PCB grid, design takes profit to avoid harmonics radiation.

## Improvements

In comparison with the first diagram proposal, 2nd \& 3rd harmonics levels can be reduced respectively as low as -27 dBc and -34 dBc by replacing L2 with a parallel tank circuit (LC) of $10 \mathrm{nH}, 13 \mathrm{pF}$. In such a condition, fundamental output level is slightly degraded of less than 0.5 dB keeping a good $50 \Omega$ impedance matching.

Figure 9 : PCB solder side (not to scale)


Figure 10 : Silk screen (not to scale)


PACKAGE MECHANICAL DATA
8 PINS - PLASTIC MICROPACKAGE (SO)


| Dim. | Millimeters |  |  | Inches |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Typ. | Max. | Min. | Typ. | Max. |
| A |  |  | 1.75 |  |  | 0.069 |
| a1 | 0.1 |  | 0.25 | 0.004 |  | 0.010 |
| a2 |  |  | 1.65 |  |  | 0.065 |
| a3 | 0.65 |  | 0.85 | 0.026 |  | 0.033 |
| b | 0.35 |  | 0.48 | 0.014 |  | 0.019 |
| b1 | 0.19 |  | 0.25 | 0.007 |  | 0.010 |
| C | 0.25 |  | 0.5 | 0.010 |  | 0.020 |
| c1 | $45^{\circ}$ (typ.) |  |  |  |  |  |
| D | 4.8 |  | 5.0 | 0.189 |  | 0.197 |
| E | 5.8 |  | 6.2 | 0.228 |  | 0.244 |
| e |  | 1.27 |  |  | 0.050 |  |
| e3 |  | 3.81 |  |  | 0.150 |  |
| F | 3.8 |  | 4.0 | 0.150 |  | 0.157 |
| L | 0.4 |  | 1.27 | 0.016 |  | 0.050 |
| M |  |  | 0.6 |  |  | 0.024 |
| S | $8^{\circ}$ (max.) |  |  |  |  |  |

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[^0]:    D = Small Outline Package (SO) - also available in Tape \& Reel (DT)

